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<p>(54) Title: VEHICLE SUSPENSION SYSTEM</p> <p>(57) Abstract</p> <p>A vehicle having a suspension comprising a double acting ram (13, 14, 17, 18) connecting each wheel (1, 2, 3, 4) independently to the body (5) of the vehicle, each ram (13, 14, 17, 18) having respective first (13a, 14a, 17a, 18a) and second (13b, 14b, 17b, 18b) chambers that vary in volume as the wheels move relative to the vehicle body (5). Each front wheel ram (13, 18) is connected to the diagonally opposite rear wheel ram (14, 17) by a respective pair of conduits (8, 10) and (8a, 10a) arranged so the first chamber (13a, 18a) of one wheel is connected to the second chamber (14b, 17b) of the other wheel. Each first and second chamber and the conduits connected thereto are filled with fluid and independent of external fluid and pressure sources. Diagonal interconnection of the front and rear rams minimizes roll movement in a lateral direction and pitch movement in the longitudinal direction of the vehicle.</p>		

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## VEHICLE SUSPENSION SYSTEM

This invention relates to a suspension system for a vehicle, and is specifically related to controlling the movement of the wheels relative to the vehicle body when turning at speed and traversing uneven surfaces.

In known suspension systems resilient means such as springs or torsion bars are provided to perform a multiplicity of functions ranging from the absorption of impact loading (as from hitting bumps at speed) to the provision of flexible support to enable all the wheels to maintain ground contact when traversing uneven terrain. Additionally applied loads such as cargo deflects traditional suspensions to induce movement between the body and wheels in a similar manner to dynamic or contour loadings.

Traditional resiliently sprung suspensions are based on each wheel assembly being provided with an individual resilient component which mechanically supports the respective "corners" of the vehicle. The resilient components have rapidly progressive load rating as deflected and normal vehicle weight is only distributed to all wheels when the wheels collectively describe a flat plane surface. When one wheel of a vehicle passes over (or is parked on) a bump, that wheel carries more vehicular weight than it normally carries on flat ground. Meanwhile the other wheels are correspondingly relieved of some of their normal share of the weight.

The rapidly progressive resiliently sprung suspension systems work satisfactorily only within a very narrow spectrum of dynamic, static and applied loading situations, and any type of overloading or even underloading of a vehicle normally adversely affects its abilities to maintain traction, average ground clearance, and quality of ride. Moreover the scope of demands upon known resilient suspension systems leads to self conflicting performance characteristics as there is no inherent ability in the system to detect and react differently to diverse situations, which cause resonant rebounding, requiring excessive damping with shock absorbers, and also anti-roll bars, thus limiting free movement of unsprung components.

Recently there has been a trend towards resilient sprung suspension systems incorporating variable damping and spring rates in an attempt to redress some of the above referred to shortcomings. Some other more advanced suspension systems (active and semi-active suspensions) incorporate a number of electronic sensors which monitor information such as vertical wheel travel and body roll, as well as speed, acceleration, steering and braking commands. This and other data is processed by a computer which instructs hydraulic actuators to override the normal function of

resilient springs in order to interpret, compensate and adjust the suspensions performance to suit speed, terrain and other factors in order to maintain a level ride and even distribution of weight onto the wheels. These suspension systems therefore require an external intelligent back-up system, and call for a substantial input of external 5 energy, drawn from the vehicle engine, to operate the actuators that effect the adjustment to the suspension system.

A range of constructions of active and semi-active suspensions for vehicles have been proposed including systems operating on the basis of compression and/or displacement of fluids and such systems currently in use incorporate a pump to 10 maintain the working fluid at the required pressure and effect distribution thereof, and sophisticated control mechanisms to regulate the operation of the suspension system in accordance with sensed road and/or vehicle operating conditions. These known systems incorporating pumps and electronic control systems, are comparatively expensive to construct and maintain, and require energy input, and therefore have limited 15 acceptability in the vehicle industry.

There has been proposed, such as in US Patent No. 4,606,551, damping systems used in conjunction with conventional sprung suspensions wherein fluid damping devices associated with individual wheels are interconnected to provide additional damping action during lateral rolling or longitudinal pitching movements. Although these 20 constructions may contribute to improved damping performance the undesirable characteristics of the basic sprung suspension, of rapidly progressive change in spring forces, lead to undesirable changes in weight distribution and limited wheel movements are still present.

It is therefore the object of the present invention to provide a suspension 25 system which eliminates the use of conventional spring components and incorporates a totally fluid suspension without the need for controlled external energy input during operation and provides unrestricted wheel movement while minimising roll and pitch motion, and is of relative simpler construction and effective in operation.

With this object in view, there is provided by the present invention a 30 vehicle having a load support body, and a pair of front ground engaging wheels and a pair of rear ground engaging wheels connected to the body to support same and each wheel being displaceable relative to the body in a generally vertical direction, a double acting fluid ram interconnected between each wheel and the body each ram including first and second fluid filled chambers on opposite sides of a ram piston, said first and second 35 chambers varying in volume in response to vertical movement between the respective

wheel and the body, each front wheel ram being connected to the diagonally opposite rear wheel ram by a respective pair of fluid communicating conduits, a first one of said pair of conduits connecting the first chamber of the front wheel ram to the second chamber of the rear wheel ram and the second one of said pair of conduits connecting the second 5 chamber of the front wheel ram to the first chamber of the rear wheel ram, each pair of conduits and the front and rear wheel rams interconnected thereby constituting a respective circuit, each said circuit incorporating resilience to accommodate fluid displaced from rams in that circuit by a resultant pressure change, each said circuit in operation being independent of external fluid and pressure sources, and said circuits 10 together minimising roll movement in a lateral direction and pitch movement in the longitudinal direction of the body.

The interaction of the interconnected pairs of diagonally opposite rams of the vehicle by virtue of the independent fluid circuits provides a control over the lateral roll of the vehicle body, as normally encountered when the vehicle is turning, 15 particularly at speed and also over fore or aft longitudinal pitch encountered during braking or acceleration of the vehicle.

The transference of the fluid medium at balancing pressures between the rams of the diagonally connected front and rear wheels effects levelling and stabilisation of the vehicle body by the extension and retraction of the appropriate rams which provide 20 the changing adjustable support mechanism of the vehicle body with reference to the unsprung wheel assemblies.

The provision of the fluid circuits interconnecting the rams of the diagonally opposite wheels as above described results in the condition whereby when any one wheel is subjected to a load attempting to move that wheel in one direction relative to 25 the body the diagonally opposite wheel attempts to move in the same direction. In operating conditions that would induce body roll or pitch in a vehicle, whereby an increase in load, on the two front or two rear wheels in the case of pitch, or on one front and one rear wheel on the same side of the vehicle in the case of roll, the presently proposed construction will inhibit pitch or roll due to the diagonally opposite wheels 30 being control-led to prevent movement in the opposite direction, and limit movements in the same direction.

In order to at least partially accommodate the displacement of fluid from the rams incorporated in each circuit, there is preferably provided at least one pressure accumulator in each fluid circuit. More specifically there is preferably at least one 35 pressure accumulator in each conduit connecting the chambers of the diagonally opposite

rams of the vehicle. The accumulators provide resilience in the suspension system as springs do in conventional vehicle suspensions.

In an embodiment of the suspension where the fluid is compressible, such as a gas, accumulators are not required as the medium is in itself an accumulator.

5 Preferably there is provided means operably interposed between the two fluid circuits and adapted to substantially equalise the pressure in the two circuits and thereby substantially equalising the loading on each wheel.

More specifically said means comprise two closed chambers each divided into two minor chambers by a respective piston, said pistons being interconnected to 10 move in unison in the respective closed chambers. The minor chambers on the same side of the respective pistons being connected respectively to the first and second conduits of one of said circuits and the minor chambers on the opposite side of the respective pistons being connected respectively to the first and second conduits of the other of said circuits, whereby in use the pistons will take up a position in the respective closed chambers to 15 equalise the pressure in the two circuits. This construction thereby provides substantial equal loading on all the four wheels.

When the vehicle is travelling on normal roadways wheel movements relative to the body are small, normally of high frequency, and are accommodated by the displacement of fluid passing into an accumulator in the connected circuit with little if 20 any transfer of fluid between ram chambers, with a resultant change in the pressure in that circuit.

However when the vehicle is off normal roadways and/or when pitch or roll creating conditions exist, larger and relative low frequency wheel movements are experienced. These are initially accommodated by some fluid passing to the accumulator, 25 with a resultant pressure rise in the circuit and some passing to other ram chambers in the circuit to induce compensating movement of the other wheel controlled by that circuit. Within a small interval of time a new stable conditions in respect to the vertical position of the wheels relative to the body is established so that the vehicle body assumes a generally horizontal or generally parallel to the overall inclination of the terrain being 30 transversed.

Unlike other suspension systems, roll and pitch minimisation and the re-establishment of body level is achieved in the presently proposed construction without the imput of energy to the suspension system, drawn from a pump, compressor or otherwise from an engine or an external power source, and without the requirement of 35 pressure transducers and other performance monitoring devices feeding information to

one or more ECUs which in turn may control electrical actuated solenoid valves, pumps, compressors or the controlled release of pressurised fluid from accumulators.

The vehicle suspension above described differs from known systems in that the wheel travel is not controlled entirely by progressive resilient suspension mechanisms and all wheels can freely follow even extremely uneven terrain. The interaction of the pressure and volume changes in the fluid circuits maintaining a substantially average vehicle body height and attitude, without unduly limiting the permissible extent of wheel travel movements. Furthermore there is an unprecedented working interrelationship between the diagonal opposite wheels which are directly interconnected to each other by the individual fluid circuits, which is collectively applied to the vehicle body so that conventional resilient components, such as springs, are not required in the suspension system. If springs are provided they can only be arranged to absorb and dampen dynamic shock, and can not inhibit the translation of wheel movement induced by uneven roads or terrain.

A vehicle supported on wheels in the above described manner allows free vertical travel of the wheels with respect to the vehicle body without having to first overcome the resistance of the conventional spring mechanisms normally incorporated between the wheels and the vehicle body. Thus, the wheels are free to move to follow the undulations of the surface being travelled without continually changing the vehicle weight distribution between the individual wheels. This substantial elimination of changes in weight distribution significantly improves the traction of the wheels to the surface being transversed and the handling characteristics of the vehicle.

Several practical applications of the present invention will now be described by way of examples with reference to the accompanying drawings.

In the drawings

Figure 1 is a diagrammatic layout of a vehicle chassis and wheel assembly incorporating the proposed suspension system.

Figure 2 is a fluid circuit diagram of a first modification of the suspension system shown in Fig 1.

Figure 3 is a fluid circuit diagram of a second modification of the suspension system.

Referring now to Figure 1 of the drawings, the vehicle chassis 5, is supported by four wheels 1 to 4 respectively through parallel wishbone type linkage 6, for front wheels 1 and 2 and trailing arms 6a for rear wheels 3 and 4, the construction of each being well known. Other known forms of linkage for connecting vehicle wheels to

a chassis could be used if preferred. It is however to be noted that no springs, torsion bars, roll or stabiliser bars or other resilient mechanical suspension elements are necessary between the chassis and the respective wheels.

A respective double acting ram is interconnected between the chassis 5 and 5 the linkages 6 and 6a connecting each wheel to the chassis. The front and rear rams on the left side in Fig. 1 are numbered 18 and 17 respectively and on the right side 14 and 13 respectively. Each of the rams have a cylinder coupled as at 50 to the chassis 5 and a piston therein dividing the cylinder into two chambers indicated as 17a and 17b in respect of cylinder 17 and 18a and 18b in respect of ram 18. The other two cylinders 10 13 and 14 are of the same construction and similarly identified. The piston of each ram is connected to the respective wheel through the linkage 6 so the piston will reciprocate in the cylinder as the wheel is moved in the general vertical direction relative to the chassis 5.

Referring now to Figures 1 and 2, the diagonally opposite rams 18 and 14 15 have the upper chamber 18a and lower chamber 14b in communication by the conduit 10 and lower chamber 18b and upper chamber 14a in communication by the conduit 8. Similarly the upper and lower chambers of the rams 17 and 13 are in communication, chambers 17a and 13b by the conduit 8a and chambers 17b and 13a by conduit 10a.

The conduits 8, 8a, 10 and 10a interconnecting the four double acting 20 rams 13, 14, 17 and 18, which support the chassis 5, each has at least one pressure accumulator 27, 21, 22 and 28 in communication therewith, and are primarily responsible for providing resilience in the suspension as do springs in most prior art sprung suspensions. If the fluid used in the rams and connecting conduits is compressible, such as a gas, accumulators are not required as the resilient medium itself 25 provides the required level of compressibility or resilience. It is preferred, as shown in Figure 2 that additional optional accumulators, are provided, such as 23, 24, 29 and 30, in each of the conduits, 8, 10, and 8a 10a respectively. These accumulators, when provided are preferably smaller and matched in size and function to the lower chambers of the rams allowing the fluid in the lower chambers to be expelled quickly and provide 30 resistance to shock loading when the wheels may be thrust down and could damage the pistons and their housings. The provision of accumulators in general also enable faster reactions and responses of ram movements as frictional losses are minimised.

All accumulators preferably are located as near as practical to their associated rams to provide an immediate and accurate response to fast dynamic forces 35 arising when the vehicle is travelling fast.

When the above described suspension is fitted to normally slow moving vehicles, such as cranes, it is appropriate to incorporate only a single accumulator in each conduit and located near the first chamber of the ram connected by that conduit. In such vehicles the accumulators may be provided with an isolating means, such as a 5 solenoid valve, to reduce the resilience of these particular circuits when under heavy load. Additionally and conversely there can be multiple accumulators in any circuit and each accumulator may be precharged with gas to a different pressure to provide a progressive variety of spring rates to suit different loading situations.

The accumulators can each be provided with damping valve in the throat 10 thereof to perform the same function as so called shock absorbers in other vehicles suspension systems.

Flow control devices such as indicated at 31, 32, 33 and 34 may be provided in any or each of the conduits reduce the rate of the fluid flow to ensure that the rams at either end of the conduits communicate directly only at a relatively slow speed, 15 as arises when the vehicle is traversing rough ground requiring large wheel travel motions, and optimum low ground pressure on all wheels. At high speeds the small dynamic wheel travel motions are best resolved primarily by the accumulators.

Any of the conduits may be provided with flow control devices of a variable nature or other means to vary and even stop the flow along the conduits between the 20 connected rams. An example of such a valve may be a solenoid valve controlled by an ECU which processes a variety of information from sources such as accelerometers or pressure transducers and thereby cause the sudden or gradual closure of the valves.

The above construction of the suspension system results in the movement of wheels 1 and 3, relative to the chassis 5, under the control of double acting rams 18 25 and 14, in the same direction due to the arrangement of the interconnecting conduits 8 and 10. The movements are also approximately equal except for such difference as may arise from the fluid passed to the accumulator or accumulators coupled to the conduits 8 and 10. The same conditions exist in respect of the wheels 4 and 3.

The above interactions between the respective rams associated with each 30 wheel of the vehicle effects control of roll when the vehicle is turning, particularly when turning at speed, and control of pitch when the vehicle is braking or acceleration, particularly severe braking or acceleration.

Figure 2 illustrates a preferred modification of the suspension system as previously described with reference to Figures 1. The basic arrangement of the double 35 acting rams 13, 14, 17 and 18 and the interconnecting conduits 8, 8a, 10 and 10a as

described with reference to Figure 1 is identical in the suspension system shown in Figure 2. Accordingly, corresponding components in Figure 2 are numbered identical to that used in Figures 1 and 2 and the construction and operations of the components will not be repeated.

5       The modification of the suspension system shown in Figure 2 resides in the load distribution unit 40 with which each of the conduits 8, 8a, 10 and 10a are in direct independent communication. The load distribution unit comprises a body 41 having in the preferred form a cylindrical bore 42 closed at each end 43 and 44 and divided into two major chambers 46 and 47 by the intermediate fixed wall 45. Respective pistons 48 and 10 49 are provided in the chambers 46 and 47 each mounted on the piston rod 51 which extends in sealed relation through the intermediate wall 45 and each closed ends 43 and 44 of the body 41.

The pistons 48 and 49 and the piston rod 51 can move in the cylindrical bore 42 providing four variable volume minor chamber 55, 56, 57 and 58, with minor 15 chambers 55 and 57 varying in the same direction in response to piston movement, and minor chambers 56 and 58 varying in the same direction but in the opposite direction to minor chamber 55 and 57 for the same piston movement. The conduits 8 and 10, forming the fluid circuit between diagonally opposite fluid rams 18 and 14, communicate with chamber 55 and 57 by branch conduits 60 and 61. Similarly conduits 20 8a and 10a, forming the fluid circuit between diagonally opposite rams 17 and 13, communicate with chambers 56 and 58 by branch conduits 62 and 63.

In the initial setting up of the suspension the fluid in the chambers 55, 56, 57 and 58 are adjusted so that the pistons 48 and 49 are each located substantially centrally in the respective major chambers 47 and 46. This initial setting up is carried 25 out with the vehicle body 5 substantially horizontal or at the preferred operating attitude; and at the preferred operating height with respect to the wheels.

When operating the vehicle if the net pressure in minor chambers 55 and 57 is greater than the net pressure in minor chambers 56 and 58 a force will exist to effect displacement of the pistons 48 and 49 upwardly as seen in Figure 2 to achieve a 30 balance between the respective net pressures. This in turn will displace fluid from chambers 56 and 58 into the respective conduits 8a and 10a to bring about a balanced pressure in all of the double acting fluid rams 13, 14, 17 and 18 thereby achieving substantially uniform load distribution between all four wheels 1, 2, 3 and 4, independent of the respective position of each wheel relative to the chassis 5.

This pressure balance between the fluid in the respective circuits is particularly achieved when variation in wheel positions is relatively large as encountered in traversing terrain of substantial irregular surface, such as encountered in off-road vehicle operation, and where wheel movement is of relatively lower frequency but of substantial magnitude. In such operating conditions, it is most desirable to retain substantially even load distribution to all wheels in order to maintain traction and prevent bogging of the vehicle. Also in such conditions it is important to reduce lateral tilting of the vehicle to improve driver and passenger comfort, and safety from rolling over of the vehicle. The load distribution unit 40 operable as above discussed affects the necessary transfer of fluid to maintain substantial even load distribution between all four wheels and reduced chassis tilting movement.

Figure 3 illustrates a preferred modification of the suspension system as previously described with reference to Figures 2. The basic arrangement of the double acting rams 13, 14, 17 and 18 and the interconnecting conduits 8, 8a, 10 and 15 10a as described with reference to Figures 1 and 2 is identical in the suspension system shown in Figure 3. Accordingly, corresponding components in Figure 3 are numbered identical to that used in Figures 1 and 2 and the construction and operations of the components will not be repeated.

Levelling of the vehicle may be achieved by pumping up the vehicle's 20 lower side while allowing fluid to drain to a reservoir from the high side. Alternatively levelling may be accomplished by either introducing or removing fluid from the circuits but by redistributing the fluid already within the circuits.

The modification of the suspension system shown in Figure 3 resides in the interconnections between the load distribution unit 40 and the conduits 8, 8a, 10 and 25 10a, which incorporates the manifold 76 between branch conduits 60, 61, 62 and 63 and load distribution unit 41. The load distribution unit as described with reference to Figure 2 includes the walls 42 and 44 and intermediate wall 45 forming major chambers 46 and 47 and pistons 48 and 49, mounted on the piston rod 51 which extends in sealed relation through the intermediate wall 45 and each closed ends 43 and 44 of the body 41. 30 However the load distribution unit 40 as shown in Figure 3 includes a further major chamber 65 through which the piston rod 51 also extends with the piston 59 mounted thereon.

The manifold 76 provides a respective straight through path for each of the branch conduits 60, 61, 62 and 63 to connect each to the respective chambers of the 35 load distribution devices 40 by the conduits 60b, 61b, 62b and 63b. It is to be noted

that conduit 60b and 62b are connected to the minor chambers 55 and 56 respectively and conduits 61b and 63b are connected to minor chambers 57 and 58. Incorporated in the manifold 76 are two change-over valves shown diagrammatically at 81 and 82. The change-over valve 81 is operable in relation to conduits 61, 61b and 63, 63b, and valve 82 operable between conduits 60, 60b and 62, 62b. Each of the change-over valves 81 and 82 may be driver operated, or automatically operated in response to sensed vehicle operating conditions. The change-over valves may conveniently be solenoid operated.

By way of illustration the change-over valve 81 is shown in Figure 3 is in the cross-over mode with conduit 60 communicating with conduit 62b and conduit 62 communicating with conduit 60b. Change-over valve 80 remains in the straight through mode with conduits 61 and 61b connected and conduits 63 and 63b connected.

The additional minor chambers 74 and 75 formed in the further major chamber 65 are connected via the manifold 76 and conduits 70, 70b and 71, 71b to the pump 78 and fluid reservoir 77 respectively, the latter being the fluid supply to the pump 78. The manifold 76 also incorporates a solenoid operated change-over valve at 83 which is operable to enable fluid to be pumped into either one of chambers 74 and 75 and to be returned from the other to the reservoir 77. Also the valve 83 is operable to short circuit conduits 70 and 71 and at the same time directly interconnect the minor chambers 74 and 75 whereby the piston 56 will not hinder the movement of the piston rod 51. The change-over valve 83 can also be driver operated or automatically operated.

While the vehicle is in normal passive use, load sharing by the wheels is accomplished by the redistribution of pressures and fluid volumes as previously described and therefore the solenoid valves within the manifold 76 remain in a position to allow the free passage of fluid to and from the associated load distribution unit 40 and the related circuits as previously described with reference to Figure 2. During such periods of operation the change-over valve 83 is positioned so the chambers 74 and 75 are directly interconnected and isolated from the pump 78 and reservoir 77.

If, however, a load is introduced into, or removed from the vehicle causing one end or side to go up or down, then the change-over valves 81 and 82 can be actuated to cause a load levelling procedure to be initiated.

By way of example, it may be desired to lower the left side of the vehicle and raise the right side and this can be accomplished by causing the piston rod 51 to move upwardly as viewed in Figure 3 by delivering fluid to minor chamber 75 by the pump 78 while the change-over valve 82 is in the position as shown in Figure 3 with conduits 60 and 62b connected, and conduits 60b and 62 connected. The vehicle can similarly be

caused to roll in the opposite direction by moving the piston rod 51 downward as seen in Figure 3 and pump fluid into minor chamber 74.

Similarly if the rear of the vehicle needs to be raised the solenoid valves within the manifold may only cross connect conduit 63 to 60b and 60 to 63b while the 5 piston rod 51 is moved upwards.

In the embodiment shown in Figure 3 the piston rod 51 can be moved by the selective admission of fluid to the minor chambers 74 and 75 from the pump 78 and this is convenient as the pump 78 can be a pump already incorporated in the vehicle such as a power steering pump. However, the piston rod 51 may be selectively moved by 10 other means such as a solenoid thereby eliminating the need for the additional major chamber 65 and piston 56 together with the associated connections to the pump 78 and reservoir 77.

It will be appreciated that if required the levelling device described may be required to work at high speed to effect vehicular attitude changes while the vehicle is 15 travelling at speed. When so operating it is preferable that the load distribution unit 40 and the associated change-over valves incorporated in the manifold 76 be controlled by electronic actuators governed by an ECU which monitors the vehicle operating conditions by appropriate sensors. In this case it is normally preferable to separate the functions of load distribution and vehicle levelling these processes may occur concurrently without 20 influencing one another.

While the accumulators described with reference to the various embodiments commonly incorporate damper valves the pneumatic version of the invention uses the volume of the chambers and connecting conduits as the resilient means itself, and the dampers normally incorporated in accumulators are therefore not 25 available. It is therefore necessary to provide separate damper units in parallel with the rams. These may be of the common telescopic shock absorber variety and can be incorporated into the rams in a variety of ways.

The double acting ram may be of forms other than the rigid cylinder and moving piston type, and, for example, may be of the flexible bellows type which do not 30 require seals as provided in the rigid cylinder type.

The bellow type being leak-free do not require provision to replace leaked fluid such as a pump, however when common double act rams are used it is optionally normal and beneficial to include a pump, compressor, accumulator or other power source to permit raising, levelling and attitude change or correction in the vehicle that may be 35 necessary as a result of fluid leakage. Some vehicles may also require the facility of

being able to run their vehicles at different and changeable heights. These variations are not illustrated or described in detail as such provisions in suspension systems are known and can easily be adapted or incorporated in the suspension system herein described.

It is to be understood that multiple axle vehicles can utilise variations of  
5 the suspension system disclosed therein and these are considered to be within the scope of the invention. Furthermore linked suspension systems which may comprise more than two circuits may usefully incorporate the technology described and therefore these variations are also included within the scope.

THE CLAIMS DEFINING THE INVENTION ARE AS FOLLOWS:

1. A vehicle having a load support body, and a pair of front ground engaging wheels and a pair of rear ground engaging wheels connected to the body to support same and each wheel being displaceable relative to the body in a generally vertical direction, a double acting fluid ram interconnected between each wheel and the body each ram including first and second fluid filled chambers on opposite sides of a ram piston, said first and second chambers varying in volume in response to vertical movement between the respective wheel and the body, each front wheel ram being connected to the diagonally opposite rear wheel ram by a respective pair of fluid communicating conduits, a first one of said pair of conduits connecting the first chamber of the front wheel ram to the second chamber of the rear wheel ram and the second one of said pair of conduits connecting the second chamber of the front wheel ram to the first chamber of the rear wheel ram, each pair of conduits and the front and rear wheel rams interconnected thereby constituting a respective circuit, each said circuit incorporating resilience to accommodate fluid displaced from rams in that circuit by a resultant pressure changer, each said circuit in operation being independent of external fluid and pressure sources and said circuits together minimising roll movement in a lateral direction and pitch movement in the longitudinal direction of the body.
2. A vehicle as claimed in claim 1 including means operably interposed between the first and second circuits and adapted to substantially equalise the pressure in said circuits and thereby substantially equalise the loading on each wheel.
3. A vehicle as claimed in claim 2 wherein said means comprises two closed chambers each divided into two minor chambers by a respective piston, said pistons being interconnected to move in unison in the respective closed chambers, the minor chambers on the same side of the respective pistons being connected respectively to the first and second conduits of one of said circuits and the minor chambers on the opposite side of the respective pistons being connected respectively to the first and second conduits of the other of said circuit, whereby in use the pistons will take up a position in the respective closed chambers to equalise the pressure in said two circuits.

4. A vehicle as claimed in claim 1 including valve means selectively operable to transfer fluid between the respective circuits to control the attitude of the vehicle body in the lateral and/or longitudinal direction.
5. A vehicle as claimed in claim 1 including means selectively operable to independently vary the volume or pressure of the fluid in each circuit to control the attitude of the vehicle body in the lateral and/or longitudinal direction.
6. A vehicle as claimed in claim 3 wherein valve means are provided to selectively communicate each conduit of the respective first and second circuits with a minor chamber on either side of the respective pistons to thereby control the attitude of the vehicle body in the lateral and/or longitudinal direction.
7. A vehicle as claimed in claim 3 or 6 including means to selectively displace said pistons in each closed chamber in unison to effect transfer of fluid between respective conduits within each circuit.
8. A vehicle as claimed in any of the claims 1 to 7 wherein each circuit has at least one pressure accumulator in communication therewith.
9. A vehicle as claimed in any of the claims 1 to 7 wherein each conduit of each circuit has a respective pressure accumulator in communication therewith.
10. A vehicle as claimed in any of the claims 1 to 7 wherein each circuit has two pressure accumulators in communication therewith, one located in proximity to each fluid ram first chamber connected to the respective conduit.
11. A vehicle as claimed in any one of the preceding claims wherein at least one conduit has a flow control means therein to control the rate of flow of fluid in either direction there through.

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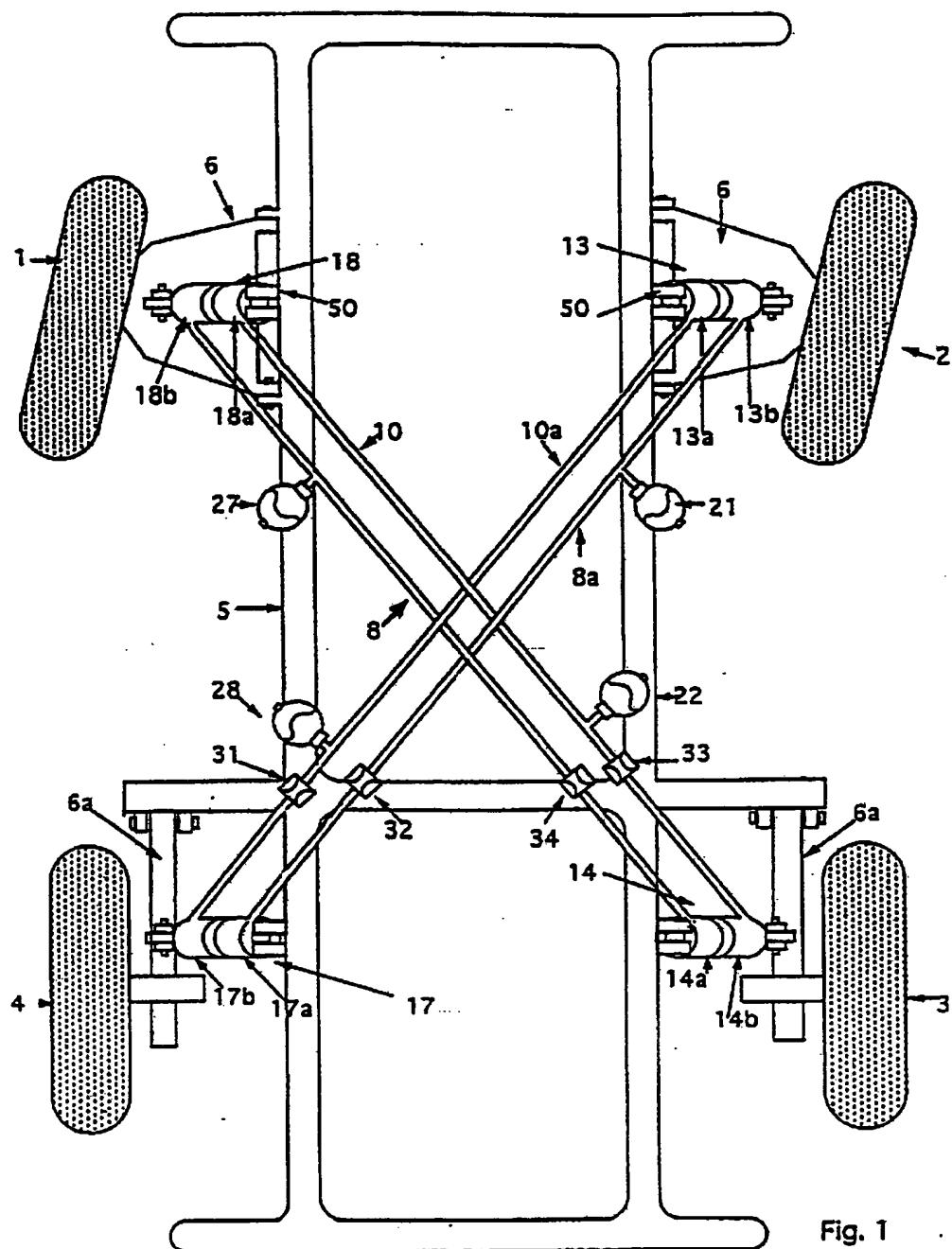


Fig. 1

2 / 3

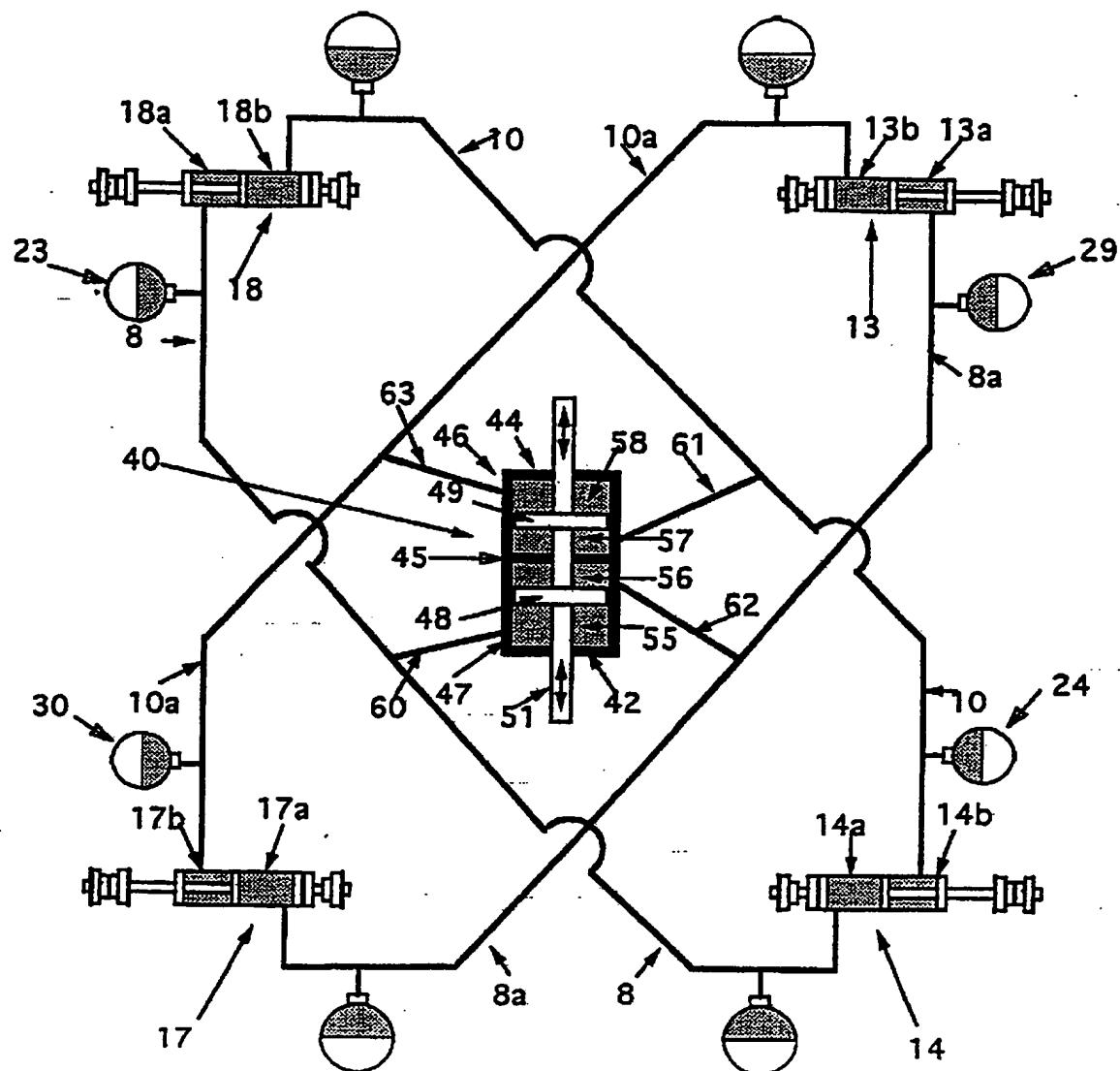


Fig. 2

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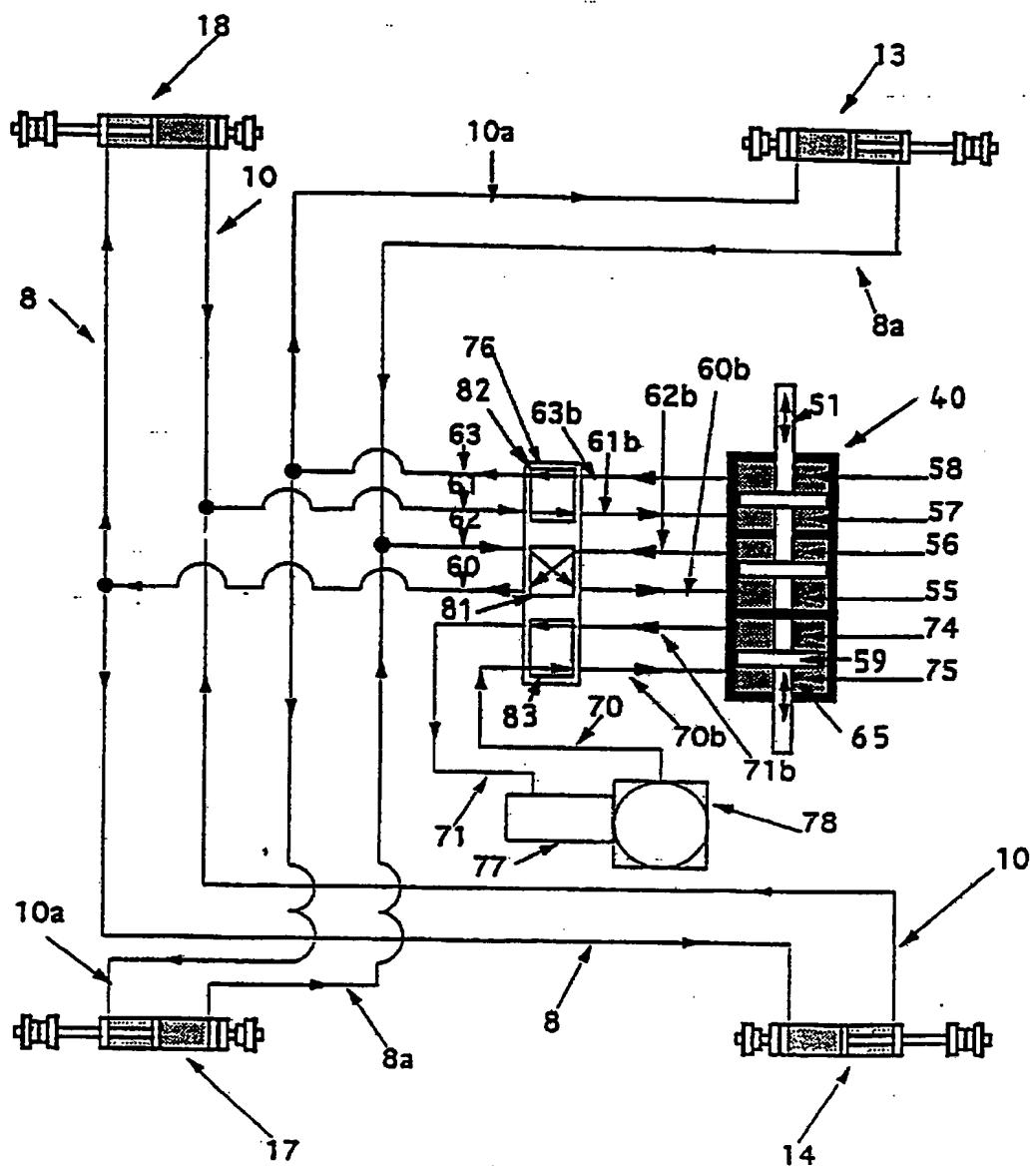


Fig. 3

**A. CLASSIFICATION OF SUBJECT MATTER**  
Int. Cl<sup>5</sup>. B60G 21/06

According to International Patent Classification (IPC) or to both national classification and IPC

**B. FIELDS SEARCHED**

Minimum documentation searched (classification system followed by classification symbols)  
IPC B60G 19/06, 19/08, 21/06

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched  
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Electronic data base consulted during the international search (name of data base, and where practicable, search terms used)  
DERWENT

**C. DOCUMENTS CONSIDERED TO BE RELEVANT**

Category	Citation of document, with indication, where appropriate of the relevant passages	Relevant to Claim No.
X	FR,A, 1535641 (INDUSTRIAL DEVELOPMENT COMPANY ESTABLISHMENTS) 1 July 1968 (01.07.68) figures 1 and 4	1, 8-10
Y	GB,A, 2009062 (NISSAN MOTOR COMPANY LTD) 13 June 1979 (13.06.79) figures 2 and 5; page 3 lines 93-101 and page 7 lines 83-90	1
Y	US,A, 3752497 (ENKE et al) 14 August 1973 (14.08.73) whole document	4

Further documents are listed  
in the continuation of Box C.

See patent family annex.

* Special categories of cited documents :	"T"	Later document published after the international filing date or priority date and not in conflict with the application but cited to understand the principle or theory underlying the invention
"A" document defining the general state of the art which is not considered to be of particular relevance	"X"	document of particular relevance; the claimed invention cannot be considered novel or cannot be considered to involve an inventive step when the document is taken alone
"E" earlier document but published on or after the international filing date	"Y"	document of particular relevance; the claimed invention cannot be considered to involve an inventive step when the document is combined with one or more other such documents, such combination being obvious to a person skilled in the art
"L" document which may throw doubts on priority claim(s) or which is cited to establish the publication date of another citation or other special reason (as specified)		document member of the same patent family
"O" document referring to an oral disclosure, use, exhibition or other means		
"P" document published prior to the international filing date but later than the priority date claimed		

Date of the actual completion of the international search 27 August 1992 (27.08.92)	Date of mailing of the international search report 18 SEP 1992 (08.09.92)
Name and mailing address of the ISA/AU AUSTRALIAN PATENT OFFICE PO BOX 200 WODEN ACT 2606 AUSTRALIA Facsimile No. 06 2811841	Authorized officer  C.M. WYATT Telephone No. (06) 2832538

C(Continuation). DOCUMENTS CONSIDERED TO BE RELEVANT		
Category	Citation of document, with indication, where appropriate of the relevant passages	Relevant to Claim No.
A	DE,A, 2135633 (MAK MASCHINENBAU GmbH) 1 February 1973 (01.02.73) figure 1	4
A	Patents Abstracts of Japan, M1032, page 5, JP,A, 2-182529 (NISSAN MOTOR CO LTD) 17 July 1990 (17.07.90) abstract	4
A	GB,A, 670361 (CALLEBAUT) 16 April 1952 (16.04.52) page 1, lines 54-59; page 2 lines 39-107 and figures 2 and 3	4
A	GB,A, 1488254 (AUTOMOTIVE PRODUCTS LIMITED) 12 October 1977 (12.10.77) page 1, line 83 to page 2, line 14 and figures 1 and 2	11

This Annex lists the known "A" publication level patent family members relating to the patent documents cited in the above-mentioned international search report. The Australian Patent Office is in no way liable for these particulars which are merely given for the purpose of information.

Patent Document Cited in Search Report	Patent Family Member		
GB,A, 2009062	DE,A, 2850912	FR,A, 2409873	US,A, 4270771
US,A, 3752497	DE,A, 2048323	FR,A, 2112232	GB,A, 1335758
DE,A, 2135633	CH,A, 535153	FR,A, 2146814	IT,A, 962908
END OF ANNEX			